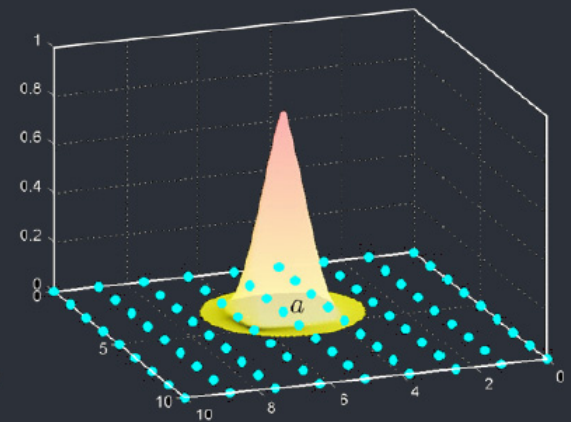
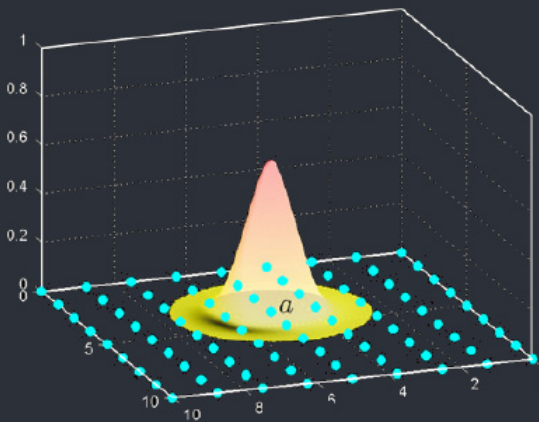
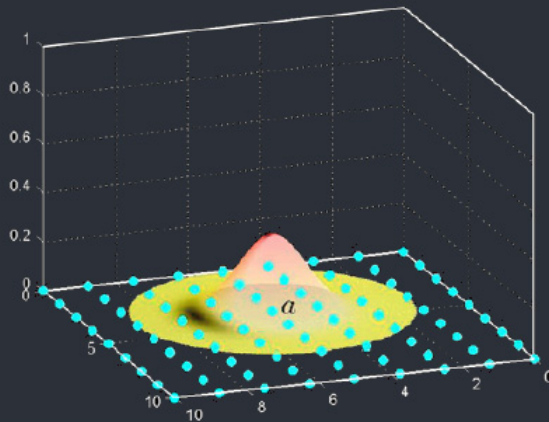


THE VIRTUAL ELEMENT DECOMPOSITION: A NEW PARADIGM FOR DEVELOPING NODAL INTEGRATION SCHEMES FOR MESHFREE GALERKIN METHODS

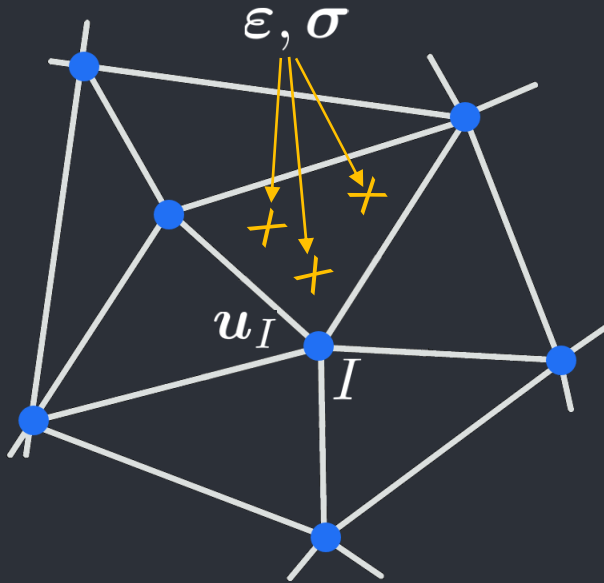


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Joint work with:
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Funded through grant CONICYT/FONDECYT No. 1181192

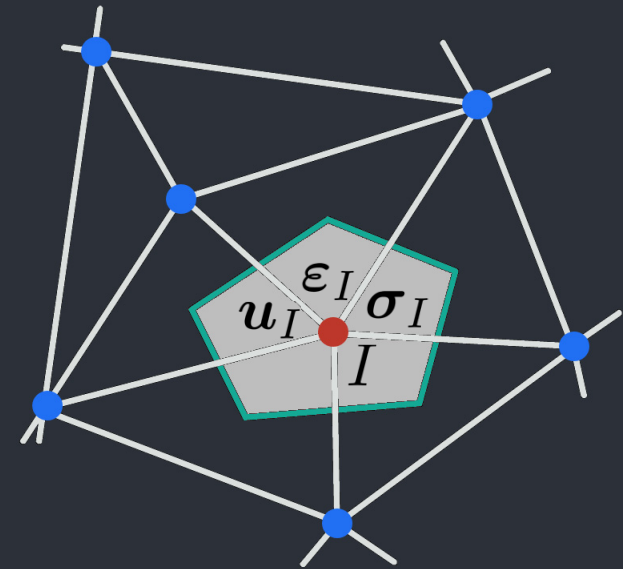
- Motivation
- Meshfree Basis Functions
- Meshfree Integration Cells
- Nodal Integration Using the Virtual Element Decomposition (NIVED)
- Numerical Tests
- Summary and Outlook



Numerical
integration of the
stiffness matrix

Gauss integration

- Displacements at nodes
- Stresses/Strains at Gauss points



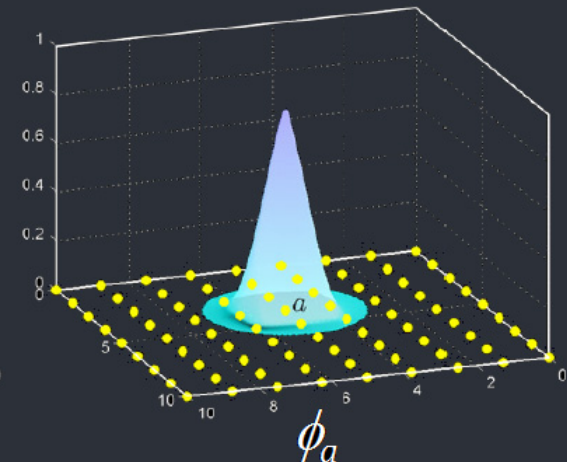
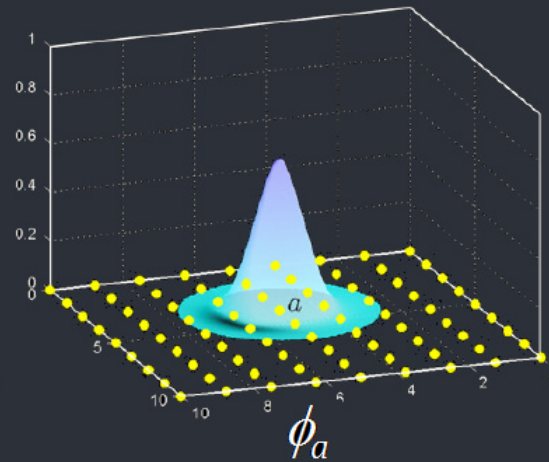
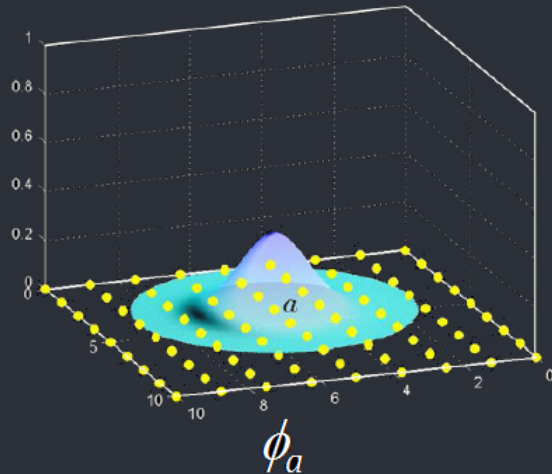
Nodal integration

- Displacements at nodes
- Stresses/Strains at nodes

Puso et al., IJNME, 74(3), 2008:

- Direct integration at nodes leads to **instabilities**
- A **penalty stabilization** is added to the stiffness matrix

Meshfree Basis Functions



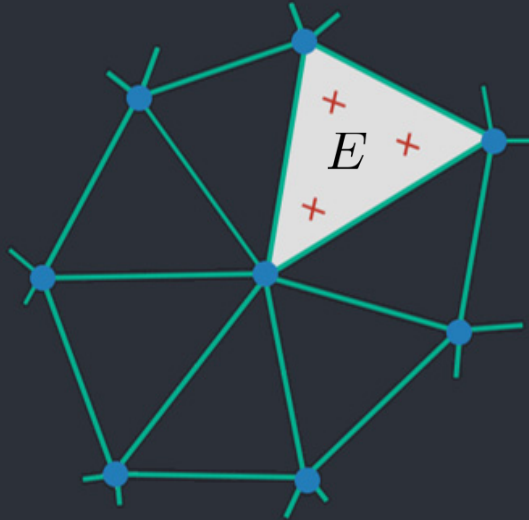
- Rational (**nonpolynomial**) basis functions
- Linear approximation plus some nonpolynomial terms
- Integration errors affecting **consistency** and **stability**

Belytschko et al., IJNME, 37(2), 1994;
Liu et al., IJNMF, 20(8-9), 1995;
Atluri & Zhu, CM, 22(2), 1998;
De & Bathe, CM, 25(4), 2000;

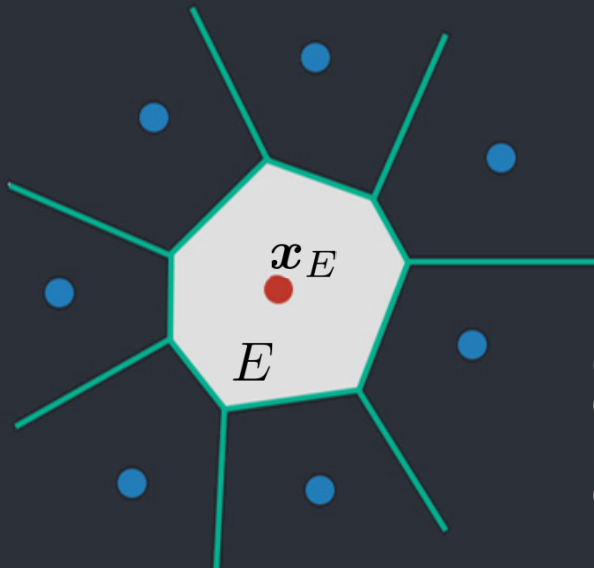
Sukumar et al., IJNME, 43(5), 1998;
Sukumar, IJNME, 61(12), 2004;
Arroyo & Ortiz, IJNME, 65(13), 2006
... and many others!

Meshfree Integration Cells

Gauss Integration

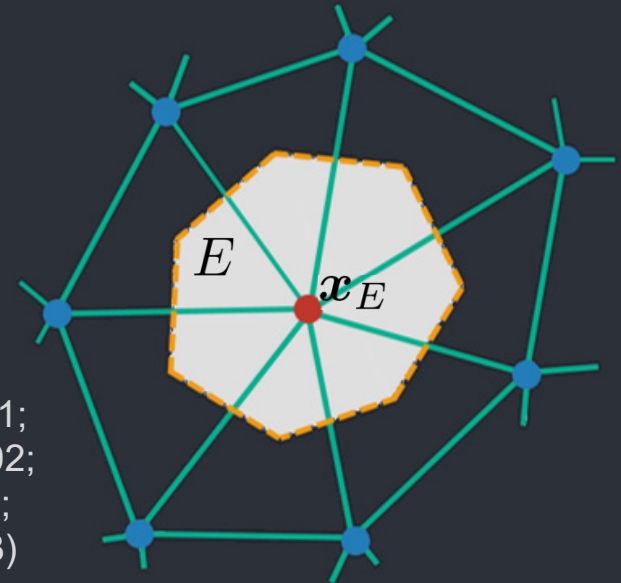


(Dolbow & Belytschko, CM, 23(3), 1999;
Babůska et al., IJNME, 76(9), 2008;
Ortiz et al., CMAE, 199(25-28), 2010;
Duan et al., IJNME, 92(4), 2012;
Chen et al., IJNME, 95(5), 2013;
Ortiz-Bernardin et al., IJNME, 112(7), 2017)



Nodal Integration

(Chen et al., IJNME, 50(2), 2001;
Chen et al., IJNME, 53(12), 2002;
Puso et al., IJNME, 74(3), 2008;
Chen et al., IJNME, 95(5), 2013)



NIVED: Basis and Spaces

Adapted from (O-B et al., IJNME, 112(7), 2017)

Bilinear form (linear elasticity) at the cell level:

$$a_E(\mathbf{u}^h, \mathbf{v}^h) = \int_E \boldsymbol{\sigma}(\mathbf{u}^h) : \nabla \mathbf{v}^h \, d\mathbf{x}$$

$$\boldsymbol{\sigma}(\mathbf{u}^h) = \mathbf{D} : \nabla_S \mathbf{v}^h$$

Approximation basis:

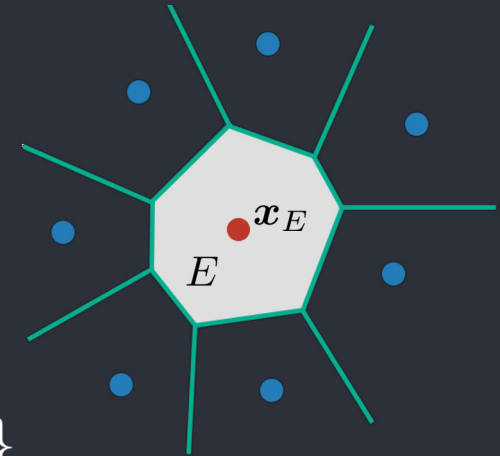
$$\mu := \{1, x, y\} \cup \{\text{nonpolynomial terms}\}$$

Displacement spaces:

$$\mathcal{P}(E) = \text{linear displacements}$$

$$\mathcal{H}(E) = \text{nonpolynomial displacements}$$

$$\therefore \mathbf{u}^h, \mathbf{v}^h \in \mathcal{W}(E) = \mathcal{P}(E) \oplus \mathcal{H}(E)$$



NIVED: Virtual Element Decomp.

Let $\Pi : \mathcal{W}(E) \rightarrow \mathcal{P}(E)$, $\Pi \mathbf{p} = \mathbf{p}$, $\forall \mathbf{p} \in \mathcal{P}(E)$. Then,

$$\mathbf{v}^h = \underbrace{\Pi \mathbf{v}^h}_{\in \mathcal{P}} + \underbrace{(\mathbf{v}^h - \Pi \mathbf{v}^h)}_{\in \mathcal{H}}$$

The projection satisfies the **orthogonality condition**

$$a_E(\mathbf{p}, \mathbf{v}^h - \Pi \mathbf{v}^h) = 0 \quad \forall \mathbf{p} \in \mathcal{P}(E), \quad \mathbf{v}^h \in \mathcal{W}(E)$$

which allows writing

$$a_E(\mathbf{u}^h, \mathbf{v}^h) = a_E(\Pi \mathbf{u}^h, \Pi \mathbf{v}^h) + a_E(\mathbf{u}^h - \Pi \mathbf{u}^h, \mathbf{v}^h - \Pi \mathbf{v}^h)$$

First term gives **consistency** and second one **stability**. The stability term can be approximated, which gives

$$a_E^h(\mathbf{u}^h, \mathbf{v}^h) := a_E(\Pi \mathbf{u}^h, \Pi \mathbf{v}^h) + s_E(\mathbf{u}^h - \Pi \mathbf{u}^h, \mathbf{v}^h - \Pi \mathbf{v}^h)$$

NIVED: Projection Operator

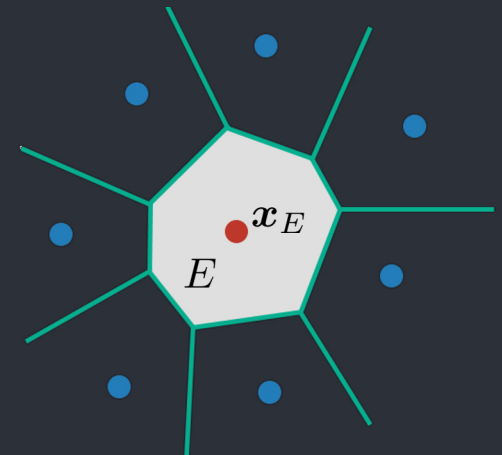
Using the “intrinsic” formula given in (BdV et al., M3A, 24(8), 2014), the projection operator sampled at \mathbf{x}_E is

$$\Pi \mathbf{v}^h(\mathbf{x}_E) = \left(\frac{1}{|E|} \int_E \nabla \mathbf{v}^h \, d\mathbf{x} \right) \cdot (\mathbf{x} - \mathbf{x}_E) + \mathbf{v}_E^h$$

where

$$\frac{1}{|E|} \int_E \nabla \mathbf{v}^h \, d\mathbf{x} = \frac{1}{|E|} \int_E \nabla_S \mathbf{v}^h \, d\mathbf{x} + \frac{1}{|E|} \int_E \nabla_{AS} \mathbf{v}^h \, d\mathbf{x}$$

$$\mathbf{v}_E^h := \mathbf{v}^h(\mathbf{x}_E)$$



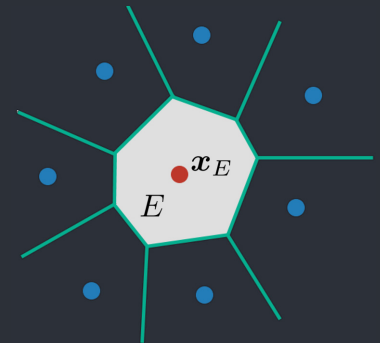
NIVED: Cell Stiffness Matrix

Virtual element decomposition:

$$a_E^h(\mathbf{u}^h, \mathbf{v}^h) := \underbrace{a_E(\Pi \mathbf{u}^h, \Pi \mathbf{v}^h)}_{\text{consistency}} + \underbrace{s_E(\mathbf{u}^h - \Pi \mathbf{u}^h, \mathbf{v}^h - \Pi \mathbf{v}^h)}_{\text{stability}}$$

Nodal integration: sampling the **consistency** part at \mathbf{x}_E and using the projection operator leads to

$$\begin{aligned} a_E(\Pi \mathbf{u}^h, \Pi \mathbf{v}^h) &= \int_E \boldsymbol{\sigma}(\Pi \mathbf{u}^h) : \nabla \Pi \mathbf{v}^h \, d\mathbf{x} \\ &= \boldsymbol{\sigma}(\Pi \mathbf{u}^h(\mathbf{x}_E)) : \nabla \Pi \mathbf{v}^h(\mathbf{x}_E) |E| \\ &= \left(\frac{1}{|E|} \int_E \nabla_S \mathbf{v}^h \, d\mathbf{x} \right) : \mathbf{D} : \left(\frac{1}{|E|} \int_E \nabla_S \mathbf{u}^h \, d\mathbf{x} \right) |E| \\ &= \mathbf{q}^\top \mathbf{K}_E^c \mathbf{d} \quad (\text{consistency stiffness}) \end{aligned}$$



Virtual element decomposition:

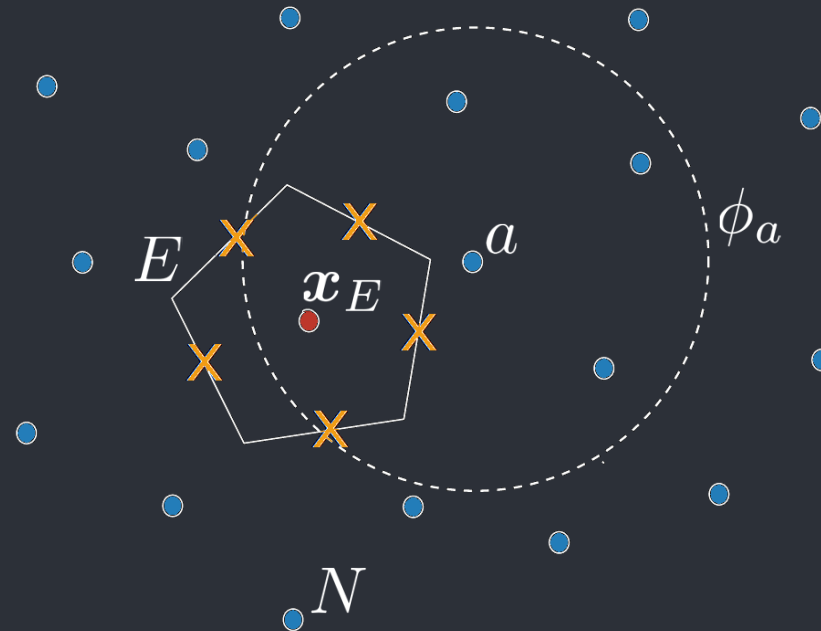
$$a_E^h(\mathbf{u}^h, \mathbf{v}^h) := \underbrace{a_E(\Pi \mathbf{u}^h, \Pi \mathbf{v}^h)}_{\text{consistency}} + \underbrace{s_E(\mathbf{u}^h - \Pi \mathbf{u}^h, \mathbf{v}^h - \Pi \mathbf{v}^h)}_{\text{stability}}$$

For the **stability** part choose s_E such that it is positive definite and scales uniformly with the exact bilinear form (e.g.: Gain et al., CMAME, 282, 2014):

$$\begin{aligned} s_E(\Pi \mathbf{u}^h, \Pi \mathbf{v}^h) &= \mathbf{q}^\top (\mathbf{I} - \Pi) \alpha_E \mathbf{I} (\mathbf{I} - \Pi) \mathbf{d} \\ &= \mathbf{q}^\top \mathbf{K}_E^s \mathbf{d} \quad (\text{stability stiffness}) \end{aligned}$$

where α_E is an scaling parameter.

NIVED: Implementation



- ● cloud of nodes (including ●) from 1 to N
- ● is the **integration point** with coordinates x_E
- E is the **integration cell** and the **representative nodal volume**
- **X** are **auxiliary integration points** on the boundary of the cell
- **Contribution**: support of ϕ_a touches the cell

NIVED: Implementation (Cont'd)

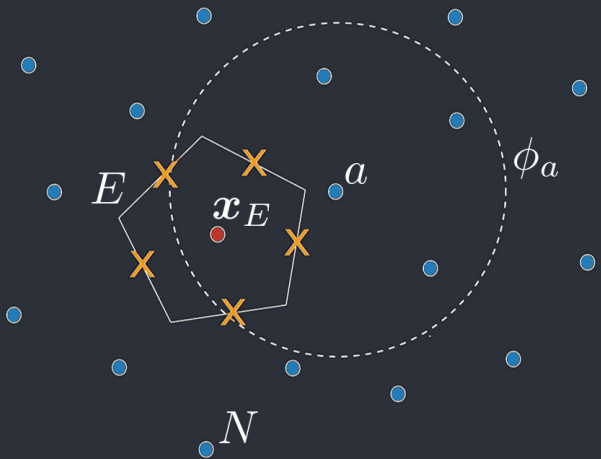
Everything reduces to the computation of the **constant strain** over the element:

$$\frac{1}{|E|} \int_E \nabla \mathbf{v}^h \, d\mathbf{x} = \frac{1}{|E|} \int_E \nabla_S \mathbf{v}^h \, d\mathbf{x} + \frac{1}{|E|} \int_E \nabla_{AS} \mathbf{v}^h \, d\mathbf{x}$$

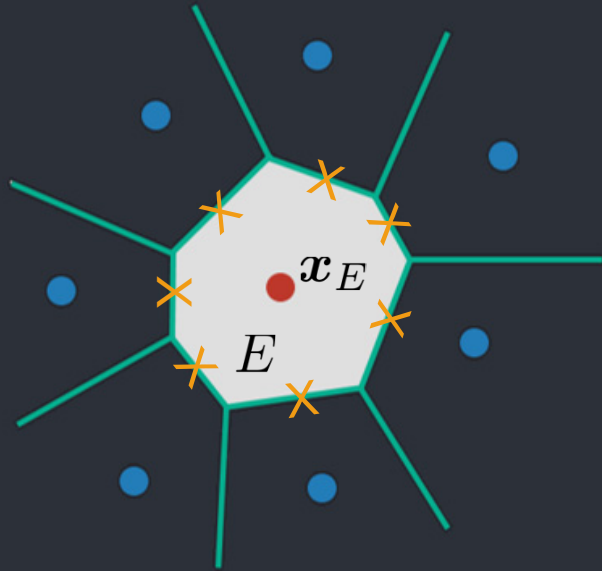
By applying the **divergence theorem**, these integrals are evaluated on the boundary of the cell:

$$\frac{1}{|E|} \int_E \nabla_S \mathbf{v}^h \, d\mathbf{x} = \frac{1}{2|E|} \int_{\partial E} (\mathbf{v}^h \otimes \mathbf{n} + \mathbf{n} \otimes \mathbf{v}^h) \, ds$$

$$\frac{1}{|E|} \int_E \nabla_{AS} \mathbf{v}^h \, d\mathbf{x} = \frac{1}{2|E|} \int_{\partial E} (\mathbf{v}^h \otimes \mathbf{n} - \mathbf{n} \otimes \mathbf{v}^h) \, ds$$



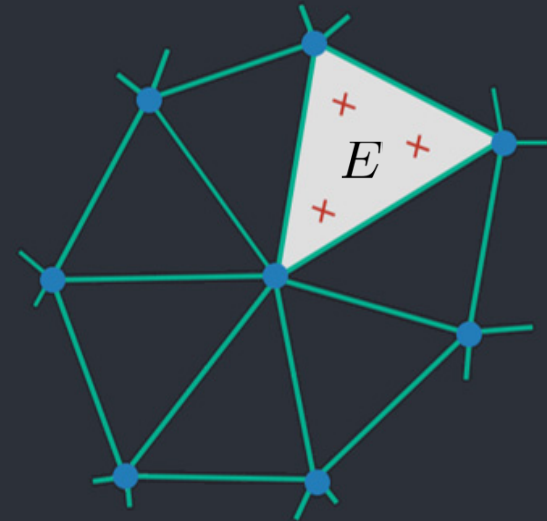
Numerical Tests: Integration Cells



NIVED

1-pt per edge
(basis function only)

Meshes use
the same
node set



MEM

Internal Gauss points:
1-pt, 3-pt, 6-pt, 12-pt
(basis functions and derivatives)

Test: Patch Test

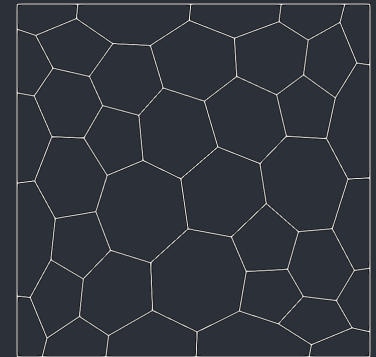
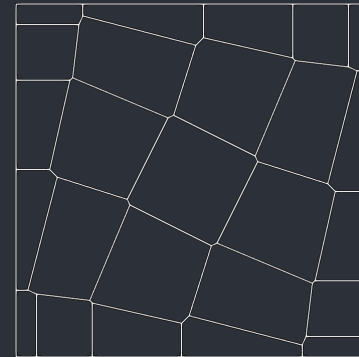
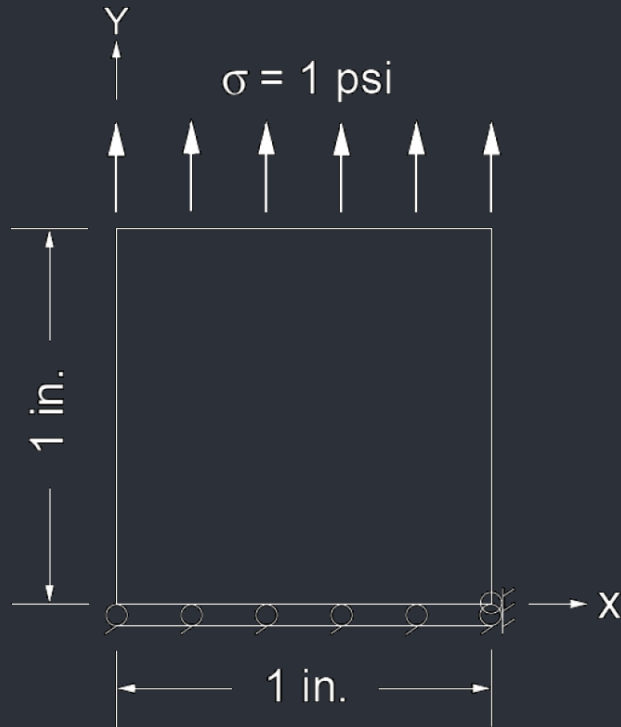


Table 1: Relative error in the H^1 seminorm

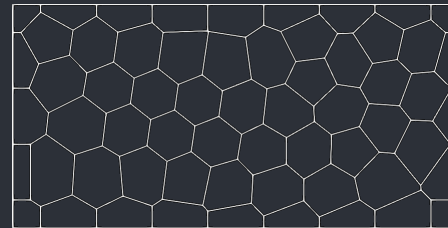
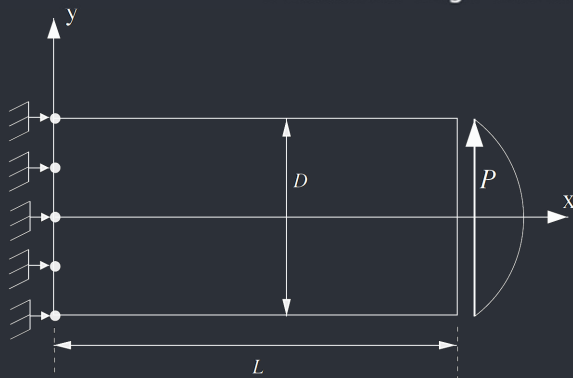
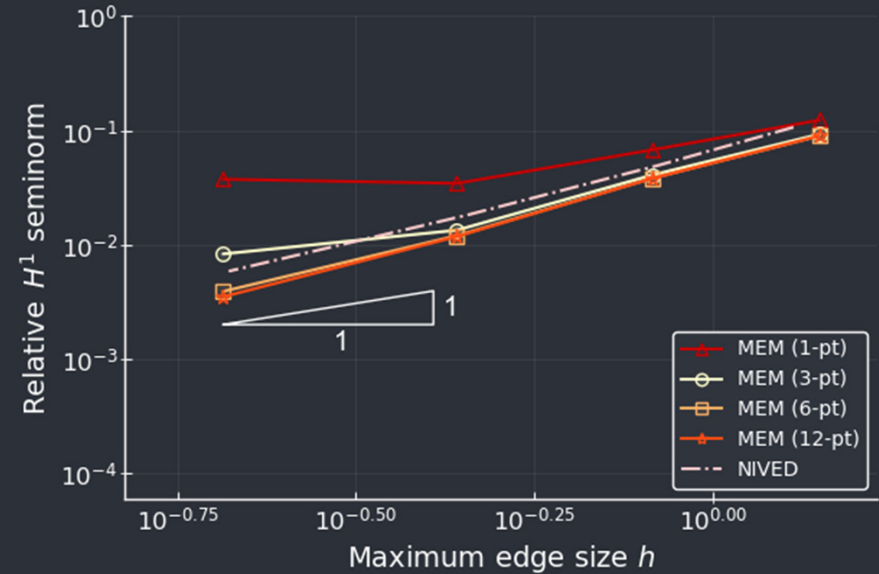
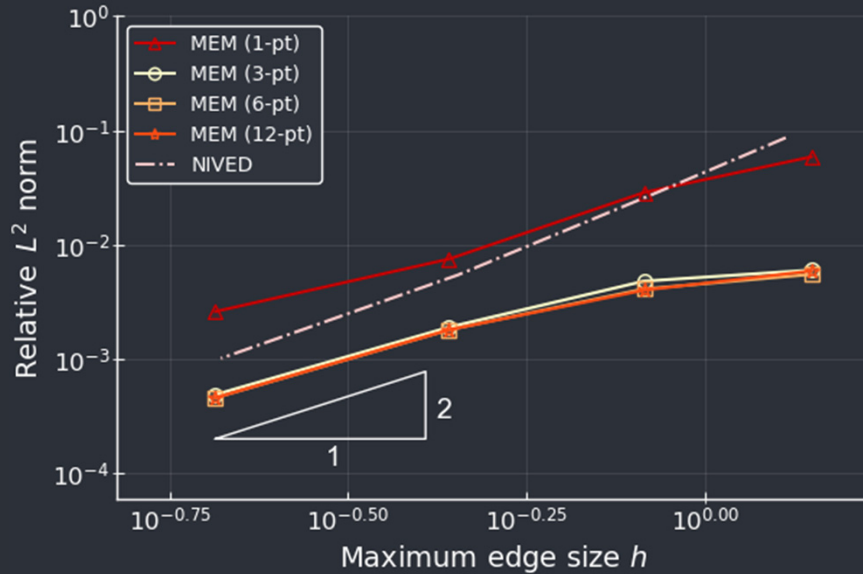
Method	Gauss rule	Regular	Distorted	Unstructured
MEM	1-pt	1.4×10^{-2}	5.4×10^{-2}	2.5×10^{-2}
MEM	3-pt	2.6×10^{-3}	5.3×10^{-3}	4.8×10^{-3}
MEM	6-pt	5.4×10^{-5}	1.9×10^{-3}	1.3×10^{-3}
MEM	12-pt	2.3×10^{-7}	7.7×10^{-4}	4.5×10^{-4}
NIVED	1-pt/edge	3.6×10^{-15}	5.2×10^{-15}	7.8×10^{-15}

Table 2: Relative error in the L^2 norm

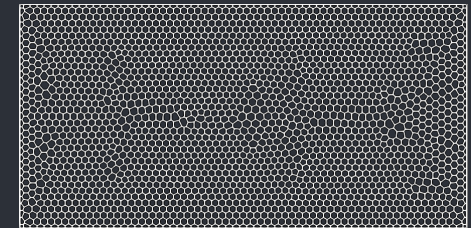
Method	Gauss rule	Regular	Distorted	Unstructured
MEM	1-pt	1.0×10^{-2}	2.0×10^{-2}	1.7×10^{-2}
MEM	3-pt	2.3×10^{-3}	1.6×10^{-3}	1.6×10^{-3}
MEM	6-pt	5.0×10^{-5}	8.0×10^{-4}	1.2×10^{-3}
MEM	12-pt	2.2×10^{-7}	3.0×10^{-4}	5.0×10^{-4}
NIVED	1-pt/edge	3.6×10^{-15}	4.1×10^{-15}	2.5×10^{-15}

Test: Cantilever Beam

Convergence



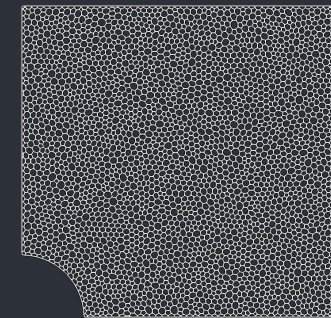
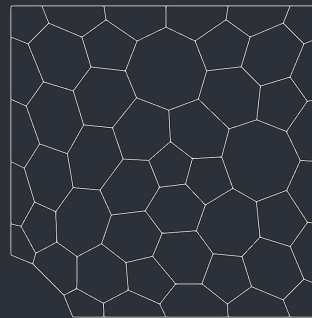
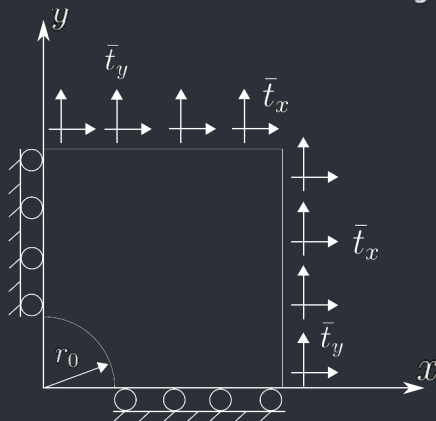
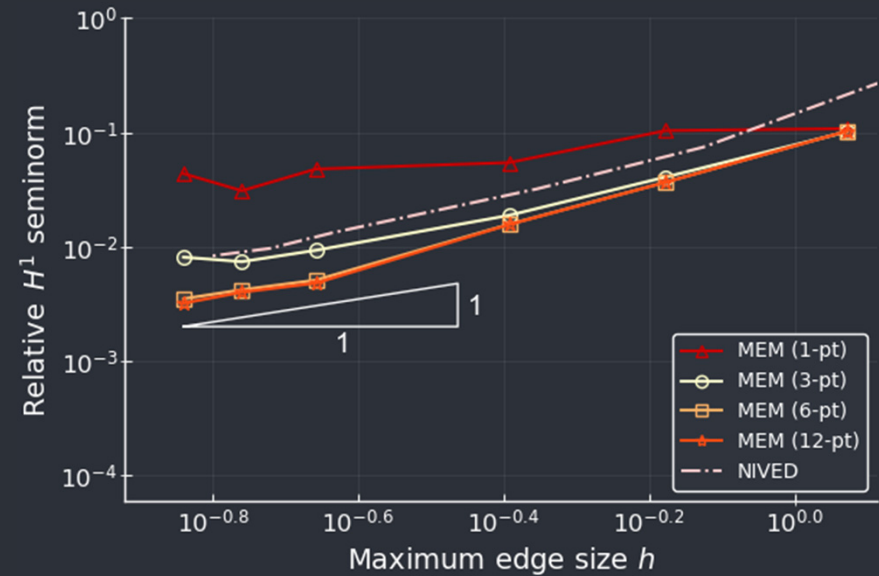
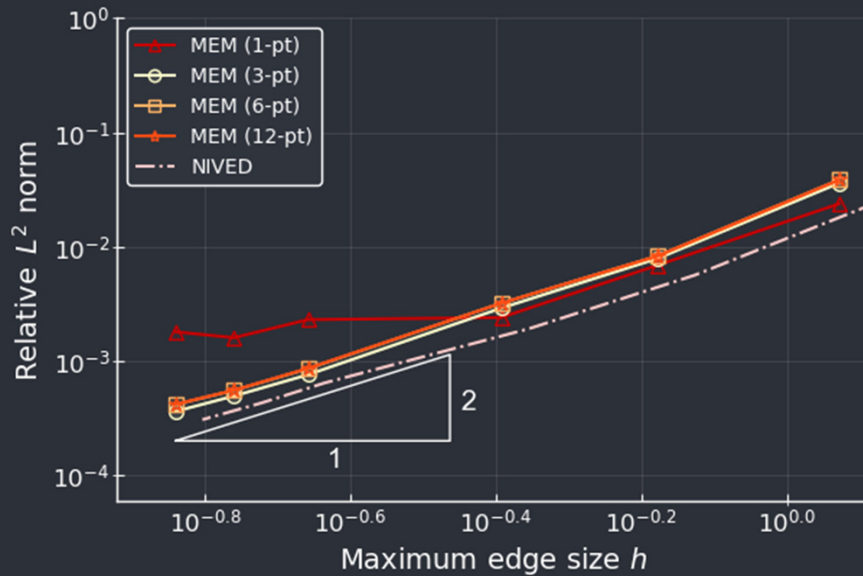
coarsest



finest

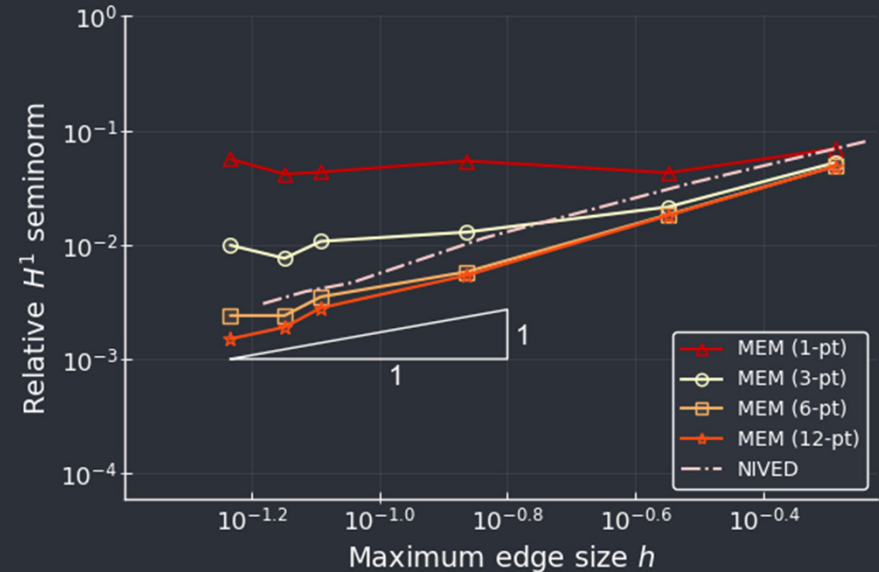
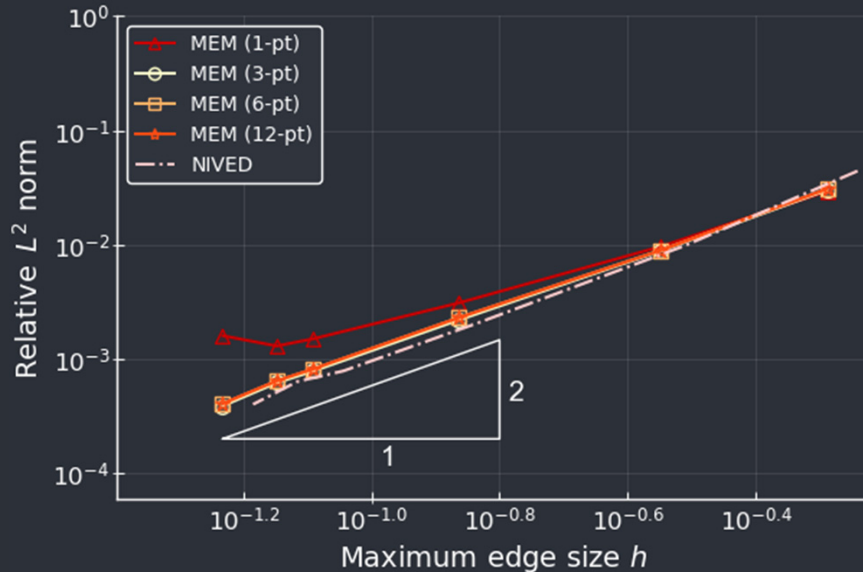
Test: Plate With a Hole

Convergence



Test: Manufactured Problem

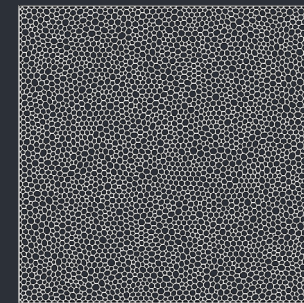
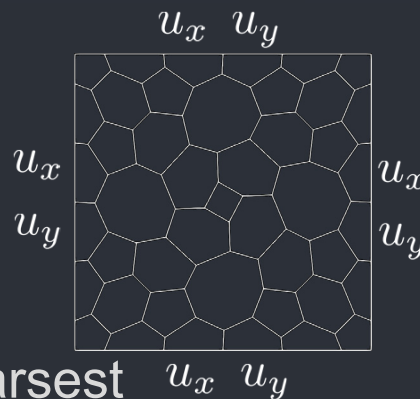
Convergence



Body force:

$$b_x = \sin x \cos y D_{11} - e^x e^y D_{12} - (e^x e^y - \sin x \cos y) D_{33}$$

$$b_y = \cos x \sin y D_{21} - e^x e^y D_{22} - (e^x e^y - \cos x \sin y) D_{33}$$



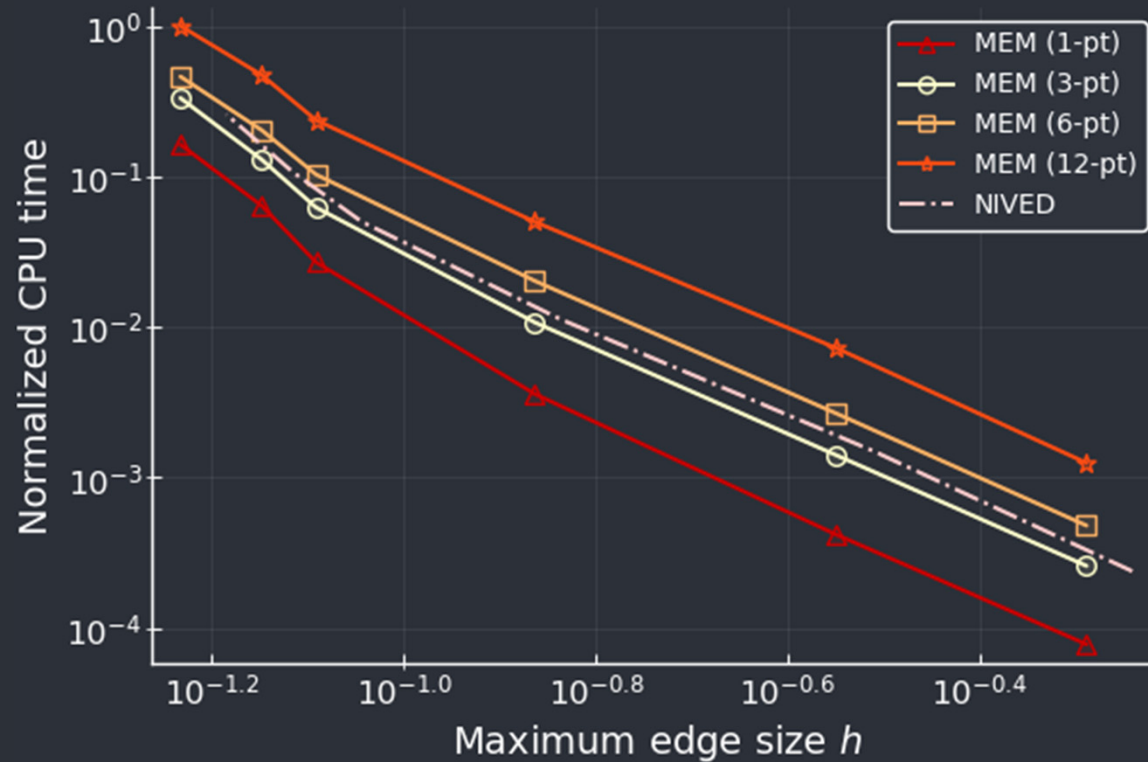
Dirichlet BCs:

$$u_x = \sin(x) \cos(y)$$

$$u_y = e^x e^y$$

Test: Manufactured Problem (Cont'd)

Timing



$$\text{Normalized CPU time} = T/T_{\max}$$

- Developed NIVED (Nodal Integration – VED) for linear elasticity
- VED provides consistency (patch test satisfaction) and optimal convergence to the nodal integration method
- Computational cost: NIVED similar to 3-pt Gauss rule
- NIVED for nonlinear problems (elastoplasticity) is under development
- Outlook: large deformations, 3D simulations

- **M3A**: Mathematical Models and Methods in Applied Sciences
- **CMAME**: Computer Methods in Applied Mechanics and Engineering
- **IJNME**: International Journal for Numerical Methods in Engineering
- **IJNMF**: International Journal for Numerical Methods in Fluids
- **CM**: Computational Mechanics